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On the Mathematics of Tunnel Fires

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Overview:

- Introduction
- Modelling
- Analysis
 - Stationary Problem
 - Transient Problem
 - Stability
- Validation of the Model
 - Tunnel on the A22
- Tunnel Networks

Background:

- 2006 Viamala Tunnel: 9 dead
- 2005 Frejus Tunnel: 2 dead
- 2001 Baltimore: 0 dead
- 2001 Gotthard Tunnel: 11 dead
- 2000 Kaprun: 155 dead
- 1999 Mont Blanc Tunnel: 39 dead
- 1999 Tauern Tunnel: 12 dead
- 1996 Euro Tunnel: 0 dead
- 1995 Baku: 300+ dead

Tunnel fires:

Typical questions:

- In which direction is the smoke going?
- How fast?
- What are the temperatures in the tunnel?
- Which is the right direction to escape?
- How can mobile ventilation systems be used?

Available software tools: (Oleinick & Carpenter ('03))

- Zone models (indoor fires)
- CFD Tools: Smartfire, Veti, Fire Dynamics Simulator, Solvent, Hitecosp, ...
- One dimensional tools: NewVendis, Camatt, Sprint,...

Problem (for long tunnels):

Relations: height/length = $10m/10km \ll 1$

- 3d (CFD) is (very) expensive.
- 3d needs many data (which often are not known).
- 3d needs a good "postprocessing".
- 3d needs a sofisticated turbulence model.
- in 3d layered air/smoke flows can be described.
- 1d modells (for mean values in the cross-section) are a good alternative.

Problem :

Chemistry of the fire:

• fire is modeled as a heat source.

2 more Problems :

Velocities: $\approx 0 - 20$ m/s Temperatures: $10^{\circ} - 2000^{\circ}$ Celsius

- Small Mach number \Rightarrow incompressible model?
- Energy transport in an incompressible model ⇒ Boussinesq approximation?
- Bussinesque approximation is only valid for small temperature differences
- Big temperature differences \Rightarrow compressible model?
- Compressible models have many problems in the small mach number regime

Model tunnel: 4 km long, $100 m^2$ crossection, 3% slope, in the middle a fire.

Buoyancy force induces an overpressure of 1.92 mbar or 19200 Newton on the upper exit.



Starting point: 1*d* compressible Navier–Stokes equations

$$\begin{split} \tilde{\rho}_{\tilde{t}} + (\tilde{\rho}\tilde{u})_{\tilde{x}} &= 0, \\ \tilde{u}_{\tilde{t}} + \tilde{u}\tilde{u}_{\tilde{x}} + \frac{1}{\tilde{\rho}}\tilde{p}_{\tilde{x}} = \eta \frac{1}{\tilde{\rho}}\tilde{u}_{\tilde{x}\tilde{x}} + \left[\tilde{p}_{l}\right] + \tilde{f}, \\ (c_{v}\tilde{\rho}\tilde{T})_{\tilde{t}} + (c_{v}\tilde{u}\tilde{\rho}\tilde{T})_{\tilde{x}} + \tilde{p}\tilde{u}_{\tilde{x}} = \lambda \tilde{T}_{\tilde{x}\tilde{x}} + \tilde{q} - \tilde{\rho}\tilde{u}\tilde{f} - \eta\tilde{u}\tilde{u}_{\tilde{x}\tilde{x}}. \end{split}$$

Variables: $\tilde{x}, \tilde{t}, \tilde{\rho} = \tilde{\rho}(\tilde{x}, \tilde{t}), \tilde{u} = \tilde{u}(\tilde{x}, \tilde{t}), \tilde{p} = \tilde{p}(\tilde{x}, \tilde{t}), \tilde{T} = \tilde{T}(\tilde{x}, \tilde{t})$

- Viscosity η , heat conductivity λ , specific heat c_v
- \tilde{f} (gravitational + external force), heat source \tilde{q} (fire)
- ideal gas law: $\tilde{p} = R\tilde{\rho}\tilde{T}$
- pressure loss in the tunnel $~ ilde{p}_l$

Dimensional analysis: Set $\tilde{a} = a_r \cdot a$

Quantity	Unit	Referencevalue	Typical Referencevalue
t	S	$t_r = L/u_r$	900 s = 15 min
x, y , z	m	L	10 ³ -10 ⁴ m
Tunnelheight	m	d	10 m
A (crosssection)	m²	A_r	10 ² m ²
u	m s $^{-1}$	u_r	1 m s ⁻¹
ρ	kg m ^{−3}	$ ho_r$	1.2 kg m ⁻³
p	kg m $^{-1}$ s $^{-2}$	p_r	1 bar $= 10^5$ kg m $^{-1}$ s $^{-2}$
f	m s ⁻²	f_r	10 m s ⁻²
T	K	$T_r = \frac{p_r}{q_r R}$	300 K
q	W m ⁻³	$q_r^{ ho_r n}$	10^{5} – 10^{6} W m ⁻³
\bar{R}	$\mathrm{m}^2~\mathrm{s}^{-2}~\mathrm{K}^{-1}$	-	287 m ² s ⁻² K ⁻¹
c_p	$\mathrm{m}^2~\mathrm{s}^{-2}~\mathrm{K}^{-1}$		1005 m ² s ⁻² K ⁻¹
η	kg m $^{-1}$ s $^{-1}$		$18 imes 10^{-6} ext{ kg m}^{-1} ext{ s}^{-1}$
λ	kg m s $^{-3}$ K $^{-1}$		$25 ext{ x } 10^{-3} ext{ kg m s}^{-3} ext{ K}^{-1}$

Machnumber M

$$M^2 = \frac{\rho_r u_r^2}{\gamma p_r} = 8.6 \cdot 10^{-6}$$

Scaled compressible NS equations I:

$$\rho_t + (\rho u)_x = 0,$$

$$u_t + uu_x + (\frac{1}{\gamma M^2}) \frac{1}{\rho} p_x = \eta \frac{1}{\rho} u_{xx} + [\overline{p_l}p_l] + \overline{f}f,$$

$$(\rho T)_t + (u\rho T)_x + (\gamma - 1)pu_x = \lambda T_{xx} + [\overline{q}q]$$

$$-M^2 \gamma (\gamma - 1) \overline{f} \rho u f - M^2 \eta u u_{xx}$$

Variables: (longitudinal) space x, time t, density $\rho = \rho(x,t)$, velocity u = u(x,t), temperature T = T(x,t), pressure p = p(x,t)

- viscosity η , heat conductivity λ , adiabatic Constant γ
- Mach number M
- ideal gas law: $p = R\rho T$

Scaled compressible NS equations II:

$$\rho_t + (\rho u)_x = 0,$$

$$u_t + uu_x + (\frac{1}{\gamma M^2}) \frac{1}{\rho} p_x = \eta \frac{1}{\rho} u_{xx} + \overline{p_l} p_l + \overline{f} f,$$

$$(\rho T)_t + (u\rho T)_x + (\gamma - 1) pu_x = \lambda T_{xx} + \overline{q} q$$

$$-M^2 \gamma (\gamma - 1) \overline{f} \rho u f - M^2 \eta u u_{xx}$$

- gravitational force $\overline{f} \cdot f = g \cdot (-\sin \alpha)$ (slope profile $\alpha(x)$)
- heat source q = q(x, t) (fire)
- pressure loss in the tunnel $\overline{p_l}p_l = -\frac{\widehat{\xi}u|u|}{d}$ (turbulence)

Scaled compressible NS equations III:

$$\rho_t + (\rho u)_x = 0,$$

$$u_t + uu_x + (\frac{1}{\gamma M^2})\frac{1}{\rho}p_x = \eta \frac{1}{\rho}u_{xx} + \overline{p_l}p_l + \overline{f}f,$$

$$(\rho T)_t + (u\rho T)_x + (\gamma - 1)pu_x = \lambda T_{xx} + \overline{q}q$$

$$-M^2\gamma(\gamma - 1)\overline{f}\rho uf - M^2\eta uu_{xx}$$

Limit $\eta \rightarrow 0 \ \lambda \rightarrow 0$

Asymptotics from Navier-Stokes to Euler (Gilbarg '51) (for travelling waves) (I.G., P.Szmolyan '93) (for travelling waves with combustion) (Wagner '89) (with combustion) Scaled compressible NS equations IV:

$$\rho_t + (\rho u)_x = 0,$$

$$u_t + uu_x + (\frac{1}{\gamma M^2})\frac{1}{\rho}p_x = \frac{\eta^2}{\rho}u_{xx} + \overline{p_l}p_l + \overline{f}f,$$

$$(\rho T)_t + (u\rho T)_x + (\gamma - 1)pu_x = \lambda T_{xx} + \overline{q_w}q_w + \overline{q}q$$

$$-M^2\gamma(\gamma - 1)\overline{f}\rho uf - M^2\eta uu_{xx}$$

Charakteristic values:

Mach number $M pprox 10^{-3} \ \Rightarrow \ arepsilon = \gamma M^2 \ll 1$

Small Mach number asymptotics:

$$p = p_0 + \varepsilon p_1 + O(\varepsilon^2)$$

momnetum balance gives

 $(p_0)_x = 0 \quad \Rightarrow \quad p_0 = p_0(t)$

Assumption: $p_0 = \text{const.}$ (leading order pressure) $T = \frac{p_0}{\rho}$

Initial boundary value problem (I.G., J.Struckmeier '02)

$$\rho_t + u\rho_x = -\rho q,$$

$$u_t + uu_x + \frac{1}{\rho}(p_1)_x = -\xi \frac{u|u|}{2} - f_d \sin \alpha$$

$$u_x = q$$

Initial values:

$$u(x,0) = u_0(x)$$
 $\rho(x,0) = \rho_0(x)$

Boundary values:

$$p_1(0,t) = p_{10}, \quad p_1(1,t) = p_{11}$$

$$u_x(0,t) = u_x(1,t) = 0$$

$$\rho(0,t) = \rho_0 (u(0,t) > 0), \quad \rho(1,t) = \rho_1 (u(1,t) < 0)$$

 ρ density, u velocity, p_1 pressure (corrections) $\alpha = \alpha(x)$ slope profile, $\xi = \xi(x)$ pressure loss, f_d scaled gravitational constant, q = q(x, t) scaled heat source Contains only one paramter (ξ) ! Asymptotical model in the 3d case: For $\overline{\eta}, \overline{\lambda}, \overline{f}, \overline{q} = O(1)$

$$\rho_t + \operatorname{div}(\rho u) = 0,$$

$$u_t + u \cdot \nabla u + \frac{1}{\rho} \nabla p_1 = \overline{\eta} \frac{1}{\rho} \Delta u + \overline{f} f,$$

$$\operatorname{div} u = \frac{\overline{\lambda}}{\overline{\gamma}} \Delta \frac{1}{\rho} + \frac{\overline{q}}{\gamma p_0} q.$$

(Majda '84, Embid '87)

Analysis

• Stationary problem (I.G. '02):

$$u\rho_x = -\rho q,$$

$$uu_x + \frac{1}{\rho}(p_1)_x = -\xi \frac{u|u|}{2} - f_d \sin \alpha$$

$$u_x = q$$

Boundary values:

$$p_1(0) = p_{10}, \quad p_1(1) = p_{11}$$

$$u_x(0) = u_x(1) = 0$$

$$\rho(0) = \rho_0 (u(0) > 0), \quad \rho(1) = \rho_1 (u(1) < 0)$$

There exist **multiple** (non-vacuum) solutions



With fire: at least two possibilities



• Transient problem I:

Reformulation

with $u(x,t) = v(t) + \int_0^x q(y,t) dy = v(t) + Q(x,t)$ and $I_f(t) = \int_0^1 f(x,t)\rho(x,t) dx$ we eliminate the pressure This gives a PDE for $\rho = \rho(x,t)$ and an ODE for v = v(t), $\rho_t + (v+Q)\rho_x = -\rho q$,

$$I v_t + I_q v + \int_0^1 \xi \rho \frac{(v+Q)|v+Q|}{2} dx = -I_{Q_t+Q_q+f_d} \sin \alpha - p_l + p_r$$

Initialdata:

$$v(0) = u_0(x) - \int_0^x q(y,0)dy$$
 $\rho(x,0) = \rho_0(x)$

Boundary data:

 $\rho(0,t) = \rho_0 (u(0,t) > 0), \quad \rho(1,t) = \rho_1 (u(1,t) < 0)$

Global existence- and uniqueness result (I.G., H.Steinrück '06)

Solutions of the type:

 $v \in C^1[0,T]$ but in ρ we have to admit discontinuities. These are natural due to the inflow conditions.

Idea of the proof:

Fixed-point- argument in the ODE Use estimates on the density from the PDE in the ODE

• Transient problem II:

Stability (I.G., H.Steinrück '06)

Stability of the solutions of the stationary problem as solutions of the transient problem,

Linear stability anaylsis gives a stability problem of a Volterra-Integro-Differential equation.

Numerical bifurcation analysis (for example depending on the pressure difference at the boundaries).

Areas of stabilty



bifurcation diagram



Example 1: Model tunnel

Length	4 km
cross-section	$100 m^2$
slope	3%
pressure loss coefficient ξ	0.1
pressure loss $p(L) - p(0)$	12.75mbar
altitude difference	14.4mbar
pressure difference (altitude corrected)	-1.65mbar
mean initial velocity	$-2.4 ms^{-1}$
heat source	5/20MW

Experiment: 28. April 2001, Brenner-highway A22





Example 2: Elbtunnel (Hamburg)

Längth	2.65 <i>km</i>	
Crosssection	$41 m^2$	
	(-3.5%)	
Slope $\alpha(x)$	$\left. \begin{array}{c} 0 \le x < 0.6km \\ -3.5\% \\ 0.6 \le x < 0.9km \end{array} \right.$	
	2.6%,	
	$0.9km \le x \le 2.65k$	
Pressure loss coefficient ξ	Ò.007	
Pressure diff. $p(L) - p(0)$	1.89mbar	
Pressure diff. (due to difference in altitude)	2.59 <i>mbar</i>	
Pressure diff.(altitude corrected)	-0.7 mbar	
Mean initial velocity	$0 m s^{-1}$	
Heatsource	15/25 <i>MW</i>	

Experiment with Turbolöscher 1999





Tunnelnetworks: (I.G., M. Kraft '04)

ventilation exits, ventilation systems, Tunnel bifurcatios etc.

Model: Graph: tunnel-pieces are the edges, bifurcations are the knodes

On the edges: one-dimensional Model for ρ, u, p .

In the knodes: mass-, momentum-, energy conservation give directly the densities for the "outflowing" tunnels . The velocities for the "outflowing" tunnels and the pressure in the knodes are unknowns. The nodes are easy to handle compared to an compressible approach.

Physically motivated monotonicity property:

increasing the pressure in a knode increases the outflow and decreases the inflow.

For explicit numerical methods in every time-step we solve a linear system for the pressures in the knodes.

Outlook

• Modeling:

variable cross-sections
big slopes
radiation
sprinkling systems
higher dimensions in regions of special interest

• Analysis:

stability small Mach number limit initial time layer problem

• Numerics: adaptive scheme